

#### DMFC DEVELOPMENT PROGRAM

- DARPA and ARO funded effort
- 150 W Portable DMFC Power System for DOD applications
  - Materials
  - Membrane-Electrode Assemblies
  - Stacks
  - Integrated Packaged Power Source



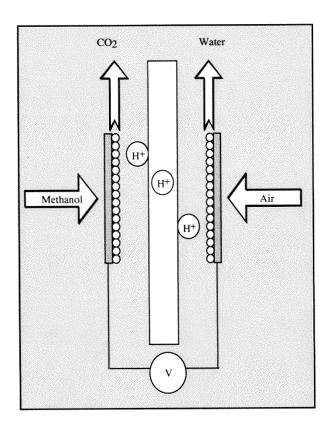
# INTRINSIC ADVANTAGES FOR SYSTEM DESIGN

#### Aqueous -Liquid Feed DMFC

- Effective Heat Removal
- More uniform stack temperature
- Reduced Complexity of Stack design
- No membrane dry out issues

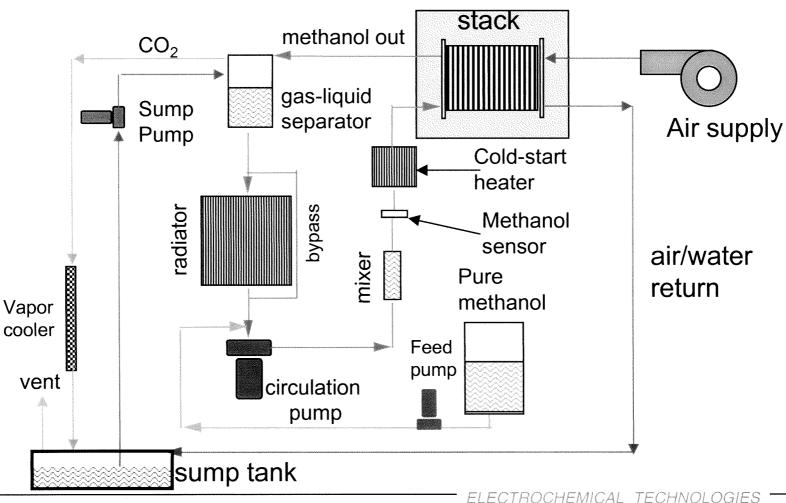
#### Direct Oxidation

- Reduces System Parts count and weight
- Reduces Control complexity



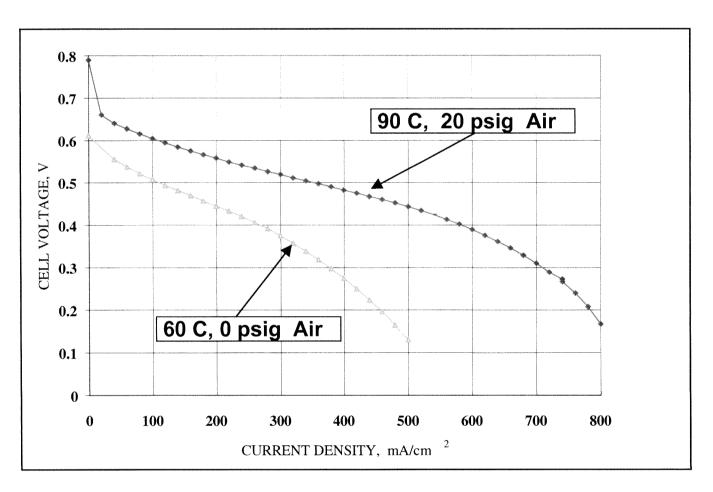


### LAYOUT OF A DIRECT METHANOL FUEL CELL SYSTEM





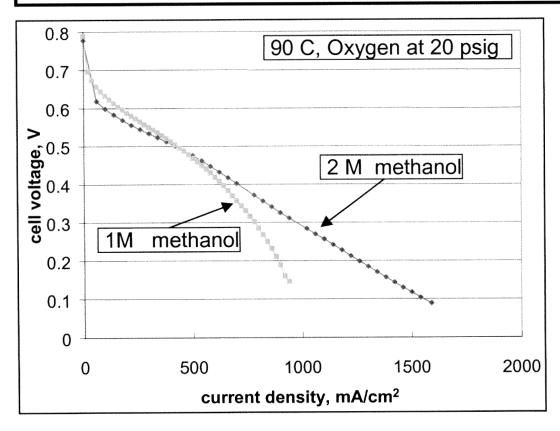
# 1M MeOH, DMFC ELECTRICAL PERFORMANCE

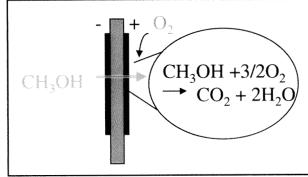


• 0.52 V at 300 mA/cm<sup>2</sup>, 0.48 V at 400 mA/cm<sup>2</sup>, Air 20 psig



# CELL PERFORMANCE WITH INCREASED METHANOL CONCENTRATION





Concentration Of Methanol	Crossover Rate@ 90 C, 0.4 V, mA/cm2
1 M	85
2 M	176

• Performance is higher. Crossover rate also higher



# ELECTROCHEMICAL FACTORS RELEVANT TO SYSTEM PERFORMANCE

ELECTROCHEMICAL FACTORS
<b>Power Density, mW/cm<sup>2</sup></b> (operating point on V-I
curve)
• Catalytic activity (Pt-Ru,)
• Ionic conductivity ( Nafion,)
Electrode/ MEA characteristics
Reactant and Product Mass Transfer
Concentration (Methanol Molarity)
• Pressure (Air)
Flow rates ( Relative to stoichiometric)
Temperature
Humidity
Flow field design features
Water handling through the stack
Electro-osmotic transport ( membrane type)
Temperature of operation
Heat generation processes
• Irreversibility (Deviation from Thermoneutral
potential)
Crossover Rate ( parasitic heat generation)
Degenerative processes
Short term stability ( for. e.g. flooding, dry out)
Long term irreversible loss (catalyst poisoning membrane degradation)



#### **CROSSOVER RATE MEASUREMENTS**

- In line CO<sub>2</sub> Analyzer; Horiba VIA-550
- Calculation
  - Convert CO<sub>2</sub> Volume % into a volume flow rate of CO<sub>2</sub>.
  - Use Ideal Gas Law to calculate a mole of CO<sub>2</sub>/sec value.

$$n = PV/RT$$
 (1)

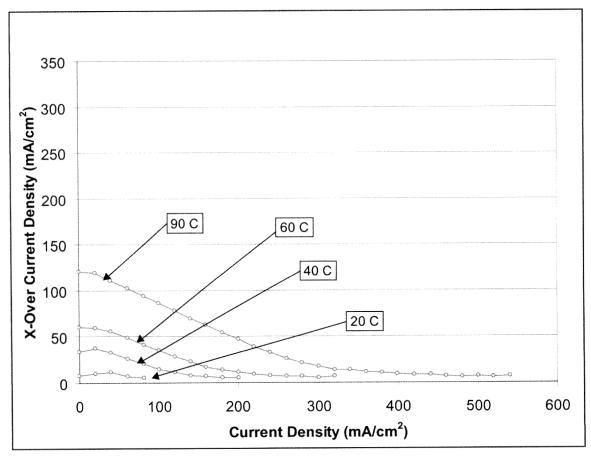
 Use Faraday's Law to calculate an effective current which can be normalized into a current density.

$$I = n Fn_e (2)$$

- Advantages of this method
  - Can see the effects of anode methanol consumption on crossover.
  - Is a true reflection of the CO<sub>2</sub> production in an operating cell.



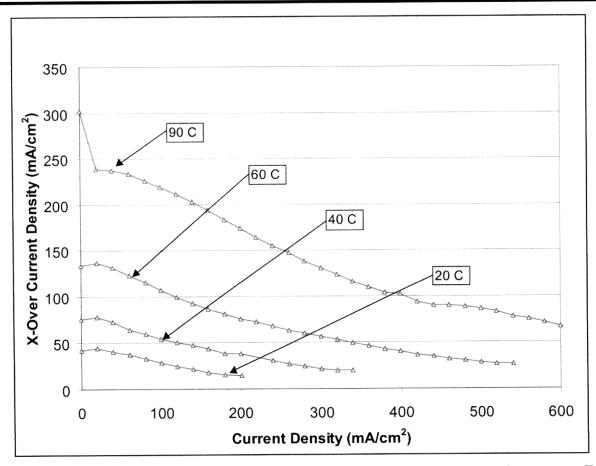
### CROSSOVER TEST, 0.5M MeOH



• Crossover Current Density Increases With Temperature.



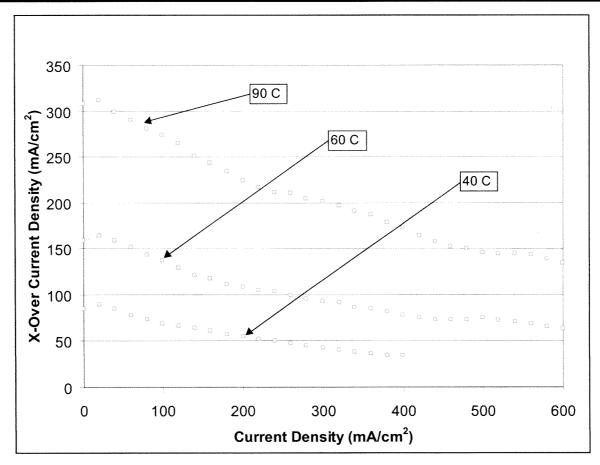
### CROSSOVER TEST, 1.0M MeOH



• Crossover Current Density Decreases With Applied Current Density.



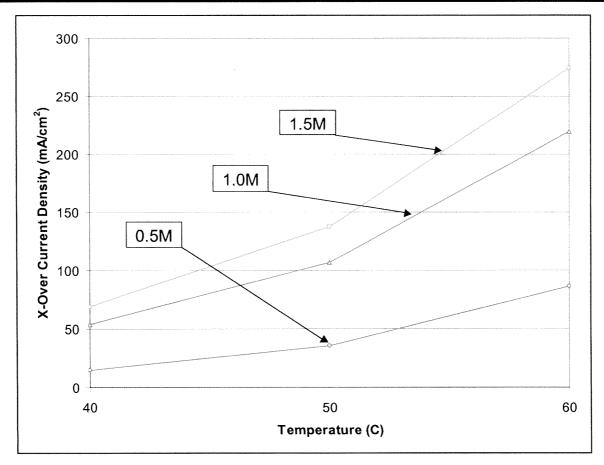
### CROSSOVER TEST, 1.5M MeOH



• Crossover Current Density Increases With Methanol Concentration.



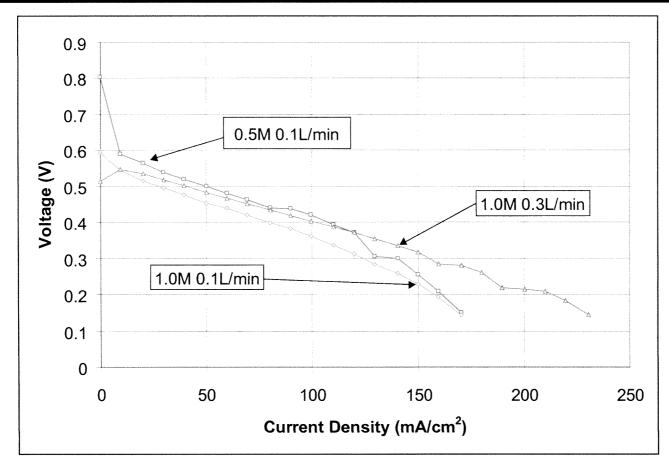
### CROSSOVER TEST, 100 mA/cm<sup>2</sup>



• Crossover Current Density Increases With Temperature and Methanol Molarity.



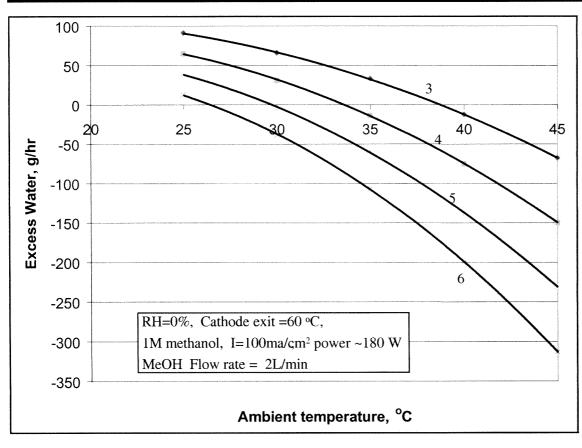
### IV PERFORMANCE, 60C MeOH

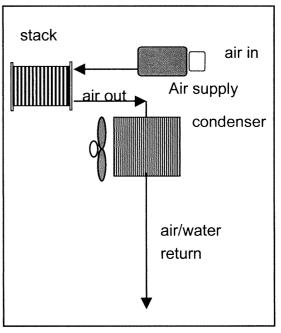


• Molarity has a greater impact on DMFC performance than airflow rate.



## EXCESS WATER RECOVERY AND ITS DEPENDENCE ON STOICHIOMETRY





• WATER BALANCE CANNOT BE ACHIEVED WITH A CONDENSER AT HIGH STOICHIOMETRY, > 37°C AMBIENT



# IMPACT OF CONDENSER DUTY ON SYSTEM SIZE AND WEIGHT

- Condensing equipment are heavy (200Wth/kg)
- Air moving equipment require power (1We/25Wth)
- Allowance for air flow through condensers
  - increased system volume
- Water handling and return
  - pumps, valves, controls, additional power demand
- IDEALLY A CONDENSER IS TO BE AVOIDED
  - Possible if the stack can be operated at very low air flow stoichiometry.



#### ANODE POLARIZATION SUBTRACTION

#### Polarization Analysis

 Ecell, at any air flow rate, can be added to Ea at the same molarity and temperature to get Ec corresponding to the flow rate.

$$E_c = E_{cell} + E_a$$
 (1)

 When E<sub>a</sub> and E<sub>c</sub> are plotted together as a function of current density, the kinetics of the reaction can be seen.

#### Cathode performance correction

- The volume percent of CO<sub>2</sub> produced at the anode can be converted into an equivalent current, I<sub>cr</sub>.
- The total current applied to the cathode becomes:

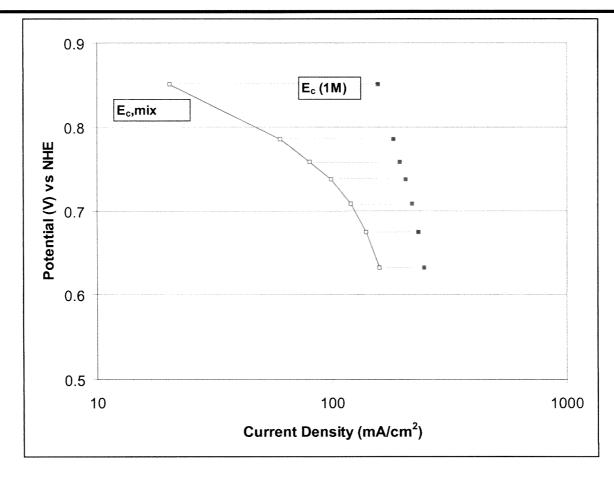
$$I_{\text{true}} = I_{\text{app}} + I_{\text{cr}}$$
 (4).

Now  $E_c$ , mix can simply be called  $E_c$ .

E<sub>c</sub> should be a constant regardless of methanol molarity.



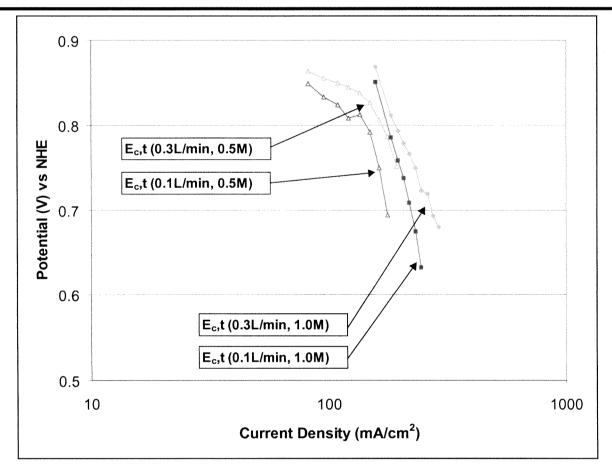
### CATHODE POTENTIALS, 60C, 0.1 L/min, AIR



• The DMFC cathode is starved for O<sub>2</sub>, when operating on 1M MeOH.



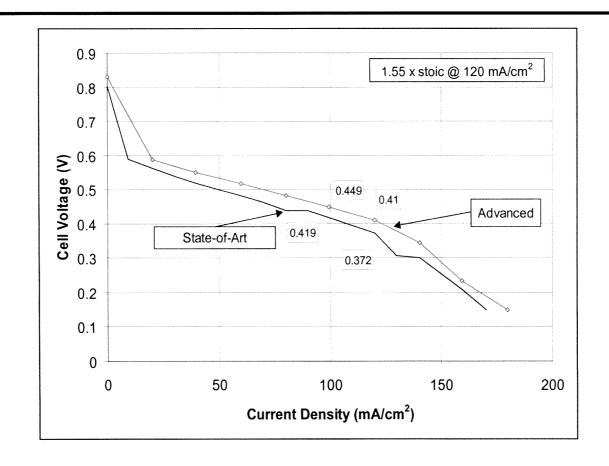
### TRUE CATHODE POTENTIALS, 60C



ullet 1.0M Methanol in  $O_2$  mass transfer limited regime regardless of airflow.



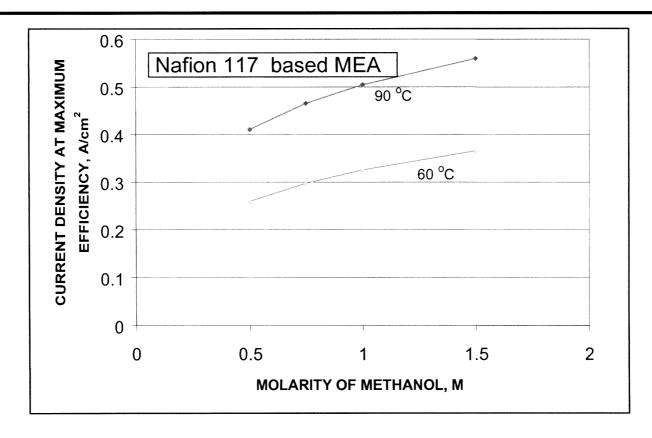
# IV COMPARISON 60C, 0.5M MeOH, 0.1 L/min, AMBIENT AIR



• A 30mV at 100 mA/cm² improvement can be achieved with a novel cathode structure.



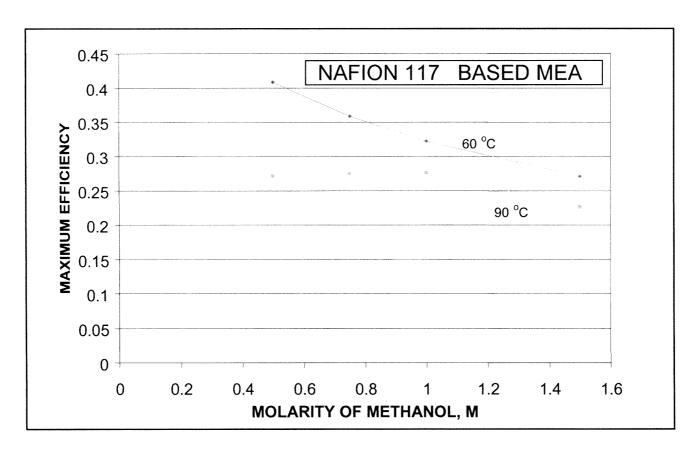
# THE CURRENT DENSITY ATTAINED AT MAXIMUM EFFICIENCY



• Current density at maximum efficiency point increases with temperature and concentration



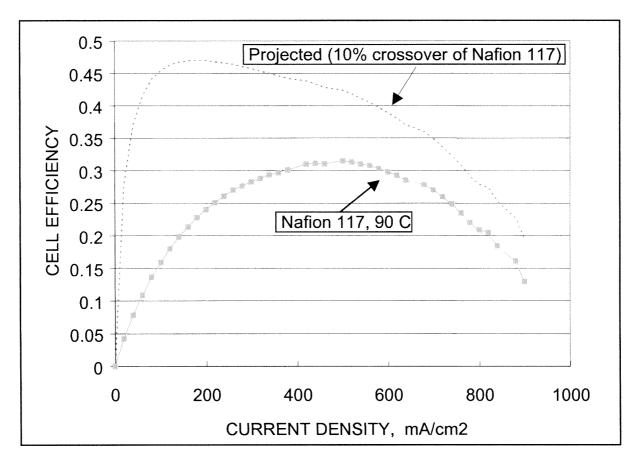
# EFFECT OF CROSSOVER AND TEMPERATURE ON MAXIMUM EFFICIENCY



• Maximum efficiency decreases with increasing temperature at all molarities



# PROJECTED IMPROVEMENT IN EFFICIENCY WITH LOW CROSSOVER MEMBRANES



•Efficiencies greater than 40% are projected with membranes exhibiting low methanol crossover



#### SUMMARY

- System Performance sensitivity very high to
  - air flow rate
  - concentration of methanol
- Air flow rate performance 1.5-1.75 x stoic
  - essential to avoid water recovery
  - extend temperature range of operation
- Operation at lower stack temperatures(60°C)
  - Will lead to higher system performance
- Concentration control necessary to achieve good system stability
  - viable methanol concentration sensor demonstrated



### Acknowledgements

- DARPA-DSO
- NASA- JPL, Caltech